INTRODUCTION

Chronic ocular diseases, such as glaucoma, uveitis, and age-related macular degeneration, are the leading causes of blindness around the world. Frequent pharmacological intervention plays a major role in the management of these diseases. Successful treatment of an ocular disease requires optimal intraocular concentration of drugs for a sufficient period of time. Some of the limitations of current methods of ocular drug delivery include physiologic and anatomic barriers, potential side effects, and poor patient compliance with the drug regimen. For example, despite the fact that eye drops account for 90% of currently accessible ophthalmic formulations, problems such as rapid drug loss in the tear meniscus and by overflow, toxic effects on ocular surfaces, anatomical constraints, and low intraocular bioavailability (less than 10%) limit the efficacy of such a topical route.

ORIGINAL ARTICLE

Mini Drug Pump for Ophthalmic Use

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ABSTRACT

Purpose: To evaluate the feasibility of developing a novel mini drug pump for ophthalmic use.

Methods: Using principles of microelectromechanical systems engineering, a mini drug pump was fabricated. The pumping mechanism is based on electrolysis and the pump includes a drug refill port as well as a check valve to control drug delivery. Drug pumps were tested first on the benchtop and then after implantation in rabbits. For the latter, we implanted 4 elliptical (9.9 x 7.7 x 1.8 mm) non-electrically active pumps into 4 rabbits. The procedure is similar to implantation of a glaucoma aqueous drainage device. To determine the ability to refill and also the patency of the cannula, at intervals of 4–6 weeks after implantation, we accessed the drug reservoir with a transconjunctival needle and delivered approximately as low as 1 µL of trypan blue solution (0.06%) into the anterior chamber. Animals were followed by slit lamp examination, photography, and fluorescein angiography.

Results: Bench-top testing showed 2.0 µL/min delivery when using 0.4 mW of power for electrolysis. One-way valves showed reliable opening pressures of 470 mmHg. All implanted devices refilled at 4–6 weeks intervals for 4–6 months. No infection was seen. No devices extruded. No filtering bleb formed over the implant.

Conclusions: A prototype ocular mini drug pump was built, implanted, and refilled. Such a platform needs more testing to determine the long term biocompatibility of an electrically-controlled implanted pump. Testing with various pharmacological agents is needed to determine its ultimate potential for ophthalmic use.

KEYWORDS: Drug delivery; Ocular; Pump; Rabbit eye; Refilling

INTRODUCTION

Chronic ocular diseases, such as glaucoma, uveitis, and age-related macular degeneration, are the leading causes of blindness around the world. Frequent pharmacological intervention plays a major role in the management of these diseases. Successful treatment of an ocular disease requires optimal intraocular concentration of drugs for a sufficient period of time. Some of the limitations of current methods of ocular drug delivery include physiologic and anatomic barriers, potential side effects, and poor patient compliance with the drug regimen. For example, despite the fact that eye drops account for 90% of currently accessible ophthalmic formulations, problems such as rapid drug loss in the tear meniscus and by overflow, toxic effects on ocular surfaces, anatomical constraints, and low intraocular bioavailability (less than 10%) limit the efficacy of such a topical route.
Systemic medications face constraints similar to those of topical medications. The high systemic doses needed to achieve adequate intraocular therapeutic levels after passing through the blood retinal barrier may result in undesired systemic side effects. After the U.S. Food and Drug Administration (FDA) approved ranibizumab injection (Lucentis; Genentech, South San Francisco, California, USA) as a treatment for neovascular age-related macular degeneration, intravitreal injections have dramatically increased, becoming one of the most common ophthalmic procedures. Patient discomfort and potential complications, such as intraocular pressure elevation, cataract formation, retinal detachment, vitreous hemorrhage, and endophthalmitis, are challenges associated with this treatment modality. Due to the limitations associated with the current methods of drug delivery (systemic, topical, and intraocular injections), attention has turned to the development of newer systems for delivery of ophthalmic solutions. These include the FDA-approved fluocinolone acetonide intravitreal implant (Retisert, Bausch & Lomb, Rochester, New York, USA) for uveitis and ongoing clinical trials with a host of other biodegradable or non-biodegradable platforms. However, a limitation of these drug delivery platforms is that they are eluting and hence provide continuous drug delivery at a set dosage and can be stopped only by explanting the device. Herein, we demonstrated the feasibility of developing a novel programmable ophthalmic mini drug pump to customize drug delivery for each patient. Moreover, the pump is refillable while implanted, and thus can deliver a variety of drugs for many years.

**MATERIAL AND METHODS**

**Device Description**

Manually- and electrically-controlled mini drug pumps were designed, fabricated, and tested using principles of microelectromechanical systems (MEMS) engineering. The manually- and electrically-controlled systems share a common layout, including a refillable drug reservoir and a transscleral cannula. The reservoir is implanted subconjunctivally, while the cannula is inserted through an incision into either the anterior or posterior segment. Dimensions for this mini drug pump were selected so that the device is easily implanted and stores enough drug to last several months without needing a refill. Biocompatible materials (silicone rubber, Parylene C, and platinum) were used to construct the prototypes.

The manually-controlled pump includes a check valve (a one-way valve) to control drug delivery. The pressure sensitive check valve is located at the tip of the cannula. It opens only when the internal reservoir pressure exceeds the check valve cracking pressure (62 kPa or 470 mmHg). The valve consists of an orifice sealed against a valve seat. Beyond the cracking pressure, the orifice lifts away from the valve seat, creating a flow path. Once driving pressure is removed, the orifice seals against the valve seat again to prevent back flow into the device.

The ability to refill with a 30 gauge needle while implanted is a novel characteristic of our device that is achieved by the resealing capability of silicone rubber. This ability significantly increases the duration over which the device can be used. Specifically, silicone rubber membranes perforated up to 24 times in the same location were leak tight even when subjected to a pressure gradient (230 mmHg). Both first generation pump prototypes are refilled through the silicone rubber reservoir wall; a refill site is not specified in these devices. The entire reservoir is made of a self-sealing material which, once punctured, can reseal. Thus, refill can be performed anywhere on the reservoir membrane.

Surgical shams and next generation pump prototypes include a designated refill port. Device refill during in vivo studies was aided by the addition of a high contrast metal refill ring in surgical shams. The refill ring (stainless steel) allowed the surgeons to visually identify and target the refill location on the device. The concept of an ocular drug delivery device and its subconjunctival placement are illustrated in Figure 1.

The first prototype mini pumps were designed to dispense drugs into the anterior chamber both...
manually and electrically, but electrolysis will be the only pumping mechanism used in the next generation of implanted devices. Precise control of delivered drug volume in manually-controlled delivery is limited by variations in the duration and force applied for depressing of the reservoir. Thus, the next generation device will utilize the same delivery paradigm but replace manual actuation with electrolysis actuation to precisely pump the desired dosage volume. Implanted batteries or wireless inductive power transfer can be used to drive electrolysis. Electrolysis is a low power process in which the electrochemically-induced phase change of water to hydrogen and oxygen gas generates pressure in the reservoir forcing the drug through the cannula (Figure 2). While voltage control is possible, current control is preferred for its direct correlation to the generated gas volume and the fluid flow rate. Either continuous or pulsatile delivery into the eye is achieved simply by adjusting the applied current. For example, a pulse of current with a specific magnitude and duration allows a bolus to be delivered; repeated application of this current waveform results in repeated bolus delivery. The length of operation required to deliver a specific dose is determined by both the magnitude and duration of the applied current, which is correlated to the flow rate. For continuous delivery, a constant current is applied to the actuator. Dosing continues until the drug is depleted.

The first generation manually-controlled mini pumps integrate a refillable reservoir (7×7×1.58 mm), suture tabs, a cannula (1×10 mm), and a check valve located at the end of the cannula (Figure 3). The manually controlled pump device consists of three joined pieces of silicone rubber. The top layer defines the chamber for the refillable drug reservoir. The middle layer defines the delivery tube and check valve orifice. The bottom layer forms the base of the device outlining the refillable chamber, delivery tube, and suture tabs. This layer contains posts and the valve seat for the check valve (Figure 4). The individual layers are bonded together after a surface treatment with oxygen plasma for 1 min. The bonds are reinforced by encapsulation with a thin layer of silicone rubber. The bonded silicone appears homogeneous, and no joined interfaces are visible.

The first electrically active drug pump is similar in layout to the mechanically-operated one. It includes an electrolysis pump (a pair of platinum interdigitated
electrodes) on a silicon base. The cannula, which is fabricated with two layers of Parylene C to form an embedded micro channel, is also integrated into the base (Figure 5).

**Bench-Top Testing and Surgical Implantation**

Bench-top and then both ex vivo and in vivo experiments were performed on the mini pumps. To investigate the performance of the electrolysis pump in the electrically-controlled device, experiments examining continuous delivery, bolus delivery, pump efficiency, gas recombination, and back pressure were conducted. Preliminary ex vivo surgical modeling in enucleated pig eyes (Siera for Medical Science, Los Angeles, California, USA) was performed, with both manually- and electrically-controlled pumps in order to evaluate the effects of surgical handling on device integrity, feasibility of surgical technique, and dispensation of trypan blue solution (0.06%, DORC International BV, Zuidland, The Netherlands) into the anterior chamber (AC). The cannula was inserted in the anterior chamber through an ~1.5 mm wide superior scleral tunnel, 2.5 mm posterior to limbus. The drug delivery tube width measured 1 mm wide to allow a suture-less closure after intraocular insertion. After depression of the reservoir with a blunt forceps or application of the current (0.5 mA) in manually- or electrically-controlled devices, respectively, trypan blue solution was dispensed through the cannula into the eye (Figure 6). Both devices were repeatedly dispensed and refilled via 30-gauge needles (Hamilton Company, Reno, Nevada, USA) through the side wall.

For in vivo testing, drug dispensation through both manually- and electrically-controlled pumps was confirmed with phenylephrine solution (1.5 and 10%, respectively; Akorn, Inc., Buffalo Grove, Illinois, USA) in rabbit eyes. All animal experiments were conducted in accordance with the Association for Research in Vision and Ophthalmology statement for the use of animals in ophthalmic and vision research and were approved by the Institutional Animal Care and Use Committee of the University of Southern California. The higher concentration of phenylephrine was used in the electrically-controlled pump to show pupillary dilation according to the calculated flow rate (2.79 ± 0.04 µL/min) in the testing time period. Surgical procedures were identical for both devices. Partial peritomy and fixing of the suture tabs to sclera with 6-0 vicryl sutures (Ethicon Inc., Johnson & Johnson Company, Somerville, New Jersey, USA) were performed before pump implantation. Under controlled lighting, the pupillary diameter of both eyes was measured in the horizontal and vertical planes to establish the baseline. By gently pressing the reservoir or applying current (0.2 mA) in the manually- or electrically-controlled pumps, respectively, 25 µL of phenylephrine solution was dispensed into the AC. The left eye was used as a control, with the same dose of phenylephrine introduced by intraocular injection. A real-time pupillary dilation was compared in both eyes in both

![FIGURE 5 Packaged electrically controlled mini drug pump.](image)

![FIGURE 6 Trypan blue solution dispensation into anterior chamber in non-electrically-controlled mini drug pump after manual pressure with blunt forceps.](image)
devices (manually-controlled: 3 mm in right eye vs. 3.5 mm in left eye, electrically-controlled: 1.5 mm in right eye vs. 3.5 mm in left eye). The phenylephrine solution was oxidized and its color changed to light brown after application of the current for electrolysis; however, activity of discolored drug was verified in a separate control experiment.

Work is in progress to develop a second-generation electrically active pump that can be configured for anterior or posterior segment drug dispensation. To optimize the design, a sham device was fabricated to provide a surgical model for refining the surgical procedure and evaluating the feasibility of refilling procedures. These devices, consisting of an elliptical reservoir with a refill port, a cannula, and suture tabs, have exterior dimensions matching the second-generation pumps (9.9 mm × 7.7 mm × 1.8 mm). Models were fabricated from silicon rubber (Figure 7). The bottom layer of the reservoir includes a sheet of polyetheretherketone (PEEK), which prevents accidental perforation of the globe during refilling (not shown in Figure 7). We implanted sham devices in 4 rabbits. Under general anesthesia and with due sterility, partial peritomy was performed. A 2-mm-wide scleral tunnel was made in the superior temporal quadrant, 2 mm posterior to the limbus. The tube was inserted into the AC after fixation of the suture tabs to the sclera with 6-0 mersiline (Ethicon Inc., Johnson & Johnson Company) (Figure 8); if leakage was observed around the tube, interrupted 8-0 vicryl sutures were used to stop the leakage. Once the device was fixed to the eye, the conjunctiva was appropriately closed with 8-0 vicryl sutures, thus, making sure the device was completely covered by conjunctiva (Figure 8, lower right). At the end of surgery, we refilled the drug reservoir via a transconjunctival injection, using a 30-gauge needle to deliver approximately as low as 1 µL of trypan blue ophthalmic solution into the AC. Topical antibiotic ointment (Rochester, New York, USA) (Neomycin-Bacitracin-Polymyxin; Bausch & Lomb) was instilled in

![Figure 7: Sham mini drug pump.](image)

![Figure 8: Surgical implantation of sham devices in rabbits. Suturing of suture tabs to sclera (upper left). Opening of AC through scleral tunnel (upper right). Insertion of cannula into anterior chamber (lower left). Suturing of conjunctiva (lower right).](image)

![Figure 9: Refilling of sham devices. Transconjunctival refilling of the device using a 30 gauge needle (left). Localizing of refill ring by transillumination (right).](image)
the fornix. To determine the ability to refill the device and the patency of the cannula and drug reservoir, at intervals of 4–6 weeks after implantation, refilling and dispensation of dye solution was repeated on a monthly basis for 4–6 months. Transillumination was used to confirm refill and to locate the metal refill ring (Figure 9).

Follow-Up Examinations

Animals were followed by slit-lamp examination for anterior chamber evaluation and indirect ophthalmoscope examination for the posterior segment every week. Intraocular pressure was checked with a Tonopen (Medtronic, Inc., Jacksonville, Florida, USA) under topical anesthesia. Diagnostic examinations included monthly anterior segment color photography and fluorescein angiography (FA) (FF 450 Plus, Carl Zeiss, Dublin, California, USA) under general anesthesia (Figure 10).

Histopathology

At the end of the last follow-up examination, the rabbits were euthanized by intracardiac injection of 2 mL of pentobarbital (Beuthanasia-D; Schering Plough Animal Health, Omaha, Nebraska, USA). The operative eye and the contralateral eye were enucleated. Each cornea was excised and sectioned into quarters. Each quarter was sectioned into two halves. One half was immersed in Davidson’s fixative solution before paraffin embedding.14 Cross sections (5 µm thick) were stained with hematoxylin and eosin for light microscopy evaluation. The other half was immersed in Karnovsky fixative to be evaluated by scanning electron microscopy (SEM) for any endothelial damage. After removal of residual fixative and dehydration through a graded series of ethanol solutions, the specimens were sputter coated with a thin layer of silver.15 The prepared specimens were examined using JEOL JSM 6390 SEM (JEOL Ltd, Tokyo, Japan). All slides were subsequently evaluated by at least three blinded knowledgeable observers.

RESULTS

Bolus delivery of trypan blue solution was demonstrated in bench-top experiments and enucleated porcine eyes with the manually-controlled surgical models. Bolus and continuous dispensation (pL/min-µL/min) suited for ocular drug delivery, with a fixed rate, were also demonstrated with the electrically-controlled device, using driving currents from 5 µA to 1.25 mA. Bench-top testing showed 2.0 µL/min delivery using 0.4 mW of power for electrolysis. Repeated dispensations were tested successfully in both groups. One-way check valves showed reliable opening pressures of 470 mmHg. Such a high opening pressure would allow refilling of the reservoir without the risk of opening the valve. The valve withstands more than 2000 mmHg of reverse pressure without leakage. Reliability of the drug reservoir following multiple refills was confirmed in bench-top experiments. Silicone rubber membranes were leak tight up to 24 times perforation in the same location even when subjected to pressure gradient (230 mmHg). There was no functional damage to the reservoir after multiple refills. We did not observe any leakage after multiple refilling in both ex vivo and in vivo experiments.

Surgical procedures were minimally invasive and well tolerated. The devices were implanted in about 60 min. All implanted devices were biocompatible and well tolerated during the 6-month follow-up period. Devices were refilled at 4–6 week intervals for a period of 4–6 months. Transconjunctival refilling was performed in less than 1 min without any complications. Anterior chamber depth and intraocular pressure were normal in all implanted eyes compared to contralateral eyes, after the surgery and after the monthly refilling. There was no retinal or optical disc damage on indirect ophthalmoscopy examination or FA (Figure 10, right).
There was neither leakage around the insertion sites nor filtering bleb formation over the implants. We did not observe any backflow from the AC into the reservoir. No cornea, iris, or lens damage was seen in slit-lamp examination, anterior color photography, or FA (Figure 10, left, middle). No infection or adverse events were observed. No devices extruded. No occlusions of cannula were noted.

Light microscopic examination of the superior temporal quadrant of cornea after staining with hematoxylin and eosin showed endothelial cell loss close to the tube site (Figure 11). The mean final corneal thickness was unchanged statistically in implanted versus control eyes (mean central corneal thickness in implanted eyes was 0.42 ± 0.02 mm vs. 0.41 ± 0.02 mm in control; mean peripheral corneal thickness in implanted eyes was 0.49 ± 0.03 mm vs. 0.51 ± 0.02 mm in control). No evidence of corneal edema was seen and epithelial integrity was uniform. However, examination of the endothelial side of the cornea by SEM revealed changes in density, size, structure, and morphology of endothelial cells in all quadrants of the cornea after 6 months. The mean endothelial cell density in the superior temporal quadrant in implanted eyes was 1348 ± 231 cells/mm² compared to 4511 ± 177 cells/mm² in control eyes and 2603 ± 214 cells/mm² in central cornea vs. 4305 ± 202 cells/mm² in control eyes. The endothelial cell changes improved significantly in one rabbit in which we ceased the refill and dispensation of trypan blue solution at 4 months after surgery (Figure 12). The mean endothelial cell density in the superior temporal quadrant was 4161 ± 278 cells/mm² compared to 4806 ± 159 cells/mm² in a control eye and 4326 ± 244 cells/mm² in central cornea vs. 4551 ± 126 cells/mm² after 6 months.

**DISCUSSION**

The new MEMS mini drug pump with refillable reservoir shows potential advantages over the current methods of ocular treatment for chronic intraocular diseases. Due to the limitations of traditional methods of treatment, there is a need for advanced ocular drug delivery systems with capability of accurate and targeted delivery.

Intraocular injections and intravitreal sustained release implants are the current therapy of choice for a variety of ocular disorders, since they achieve therapeutic concentrations while bypassing the physi-
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Sustained-release implants (biodegradable or non-biodegradable) allow continuous drug release over an extended period of time. These devices contain a fixed concentration of drug specially formulated for release at a fixed rate; but after implantation, there is no way to change the drug, its concentration, or its release rate. Nor can these devices be refilled. Once the drug is expended, the implant must be surgically removed and replaced. Sustained-release implants are limited by safety concerns and lack of precision in the erosion rate.

Of the three types of drug delivery systems (biodegradable or non-biodegradable implants, implantable pump systems, and atypical implantable systems), those that are categorized in either the first or the third group have had limited application. No implantable pump systems for ocular drug delivery have been developed to date because of the inability to simultaneously miniaturize them and achieve low power operation.

The use of MEMS technology allows integration of highly functional electronic and fluidic systems in biomedical platforms for biomedical applications. The advantages of MEMS fabrication for producing miniaturized and efficient drug delivery systems have already been realized for delivery of insulin and for delivery of bioactive compounds to neural tissues. MEMS fabrication allows the device to be miniaturized to facilitate surgical implantation and uses materials with a proven biocompatible track record. To our knowledge, this is the first implantable ocular MEMS mini drug pump that is refillable, enables long-term use, and possesses broad drug compatibility. Furthermore, the device contains a flow control valve and a transscleral cannula for directed delivery in either the anterior or posterior segment while minimizing dose volume and increasing drug bioavailability. These advantages can increase patient comfort and reduce the complications observed with intraocular injections.

The system integrates electrolysis pumping for automated and programmable dosing, thus drug delivery can be changed in the future by software, and the loss of efficacy related to poor patient compliance will be minimized. The flow rate can be set simply by changing the applied current. This allows bolus or continuous pumping as well as variation in flow rate. For long-term use and to prevent electrolysis-generated gases from escaping into the eye during delivery, the electrolysis pump and drug reservoir will be separated in second generation devices. They will be mechanically coupled through a flexible diaphragm to allow pumping. This design prevents from oxidation of the drug and its undesirable local pH effects as observed in our phenylephrine solution dispensation experiments.

Other concerns may arise during and after surgical implantation, which must be considered. Infection may develop; but we did not see this in our animal trial despite monthly transconjunctival refilling. Also, in general, the infection rate of other drug pumps in the body, such as the insulin pump, was reported with a range of 0.06 to 0.27 infection events per patient per year. Similar to the preparation for an intraocular injection, the fornix should be sterilized with a drop of 5% povidine-iodine and aseptic technique should be practiced during refilling of the pump to reduce the risk of any infection. If the check valves become clogged, the elevated pressure generated by electrolysis should easily purge the valve open. Similar to a glaucoma aqueous drainage device, proper placement of the tube in the AC is important to reduce any traumatic damage to the corneal endothelium, iris, pupillary margin, and lens. Careful placement of the tube into the posterior segment will prevent complications, such as lens damage and retinal detachment. Corneal endothelial cell damage is one of the adverse complications of glaucoma drainage device implantation, such as Ahmed glaucoma valve. Our histological examinations in implanted eyes showed similar results, although the mechanism is not fully understood. Corneal endothelial cell density was previously assessed after Ahmed glaucoma valve implantation and mean percentage cell loss from the baseline were reported to range from 3.5% at 1 month to 10.5% at 12 months after surgery. Trauma to the endothelium reduces cell density, increases cell size, and disrupts the normal morphological pattern. Continued small movements of the tube element relative to the cornea, intraoperative and early postoperative damage caused by macroscopic contact of tube with the cornea in association with poor positioning of a long tube, or anterior chamber shallowing are among the most common causes of this damage. These findings indicate that particular care should be taken during the fabrication and implantation of the device to provide a shorter beveled tube with a smoother tip to decrease endothelial damage. In addition to the above hypothesis, as Van Dooren and his coworkers demonstrated, trypan blue (0.06%) toxicity could be another cause of corneal endothelial cell damage in our study. Generalized endothelial changes in all quadrants of the cornea after monthly refilling and dispensation of trypan blue solution for 6 months and improving of endothelial cells to almost normal shape, size, and density in one of the rabbits, which we stopped the refilling
4 months after surgery, support this hypothesis as well.34–37 We are undertaking more animal implantations without trypan blue application to further evaluate the degree to which corneal changes were mechanical related to the AC tube versus chemical toxicity due to trypan blue solution.

In conclusion, a prototype mini drug pump for the eye was built, implanted and refilled while in place. It provides a platform for more effective drug treatment for chronic ocular diseases due to controlled, programmable drug delivery. Such a platform with integrated valves and electrolysis pump in second generation devices needs to be tested in vivo to determine its long-term biocompatibility and to test its use with various pharmacological agents to determine its ultimate potential for ophthalmic use.

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Declaration of interest: Dr. Humayun and Dr. Varma are consultants and have equity in Replenish Inc. All authors except Dr. Varma stand to get royalties through University of Southern California patents licensed to Replenish Inc.

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